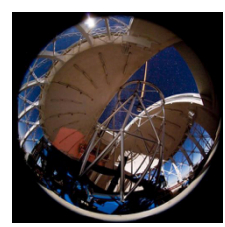


# Rejecting Harmonic Vibrations

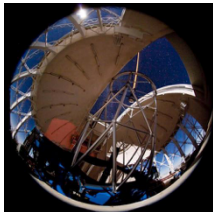
With Real-Time Frequency Tracking at M2



# Overview

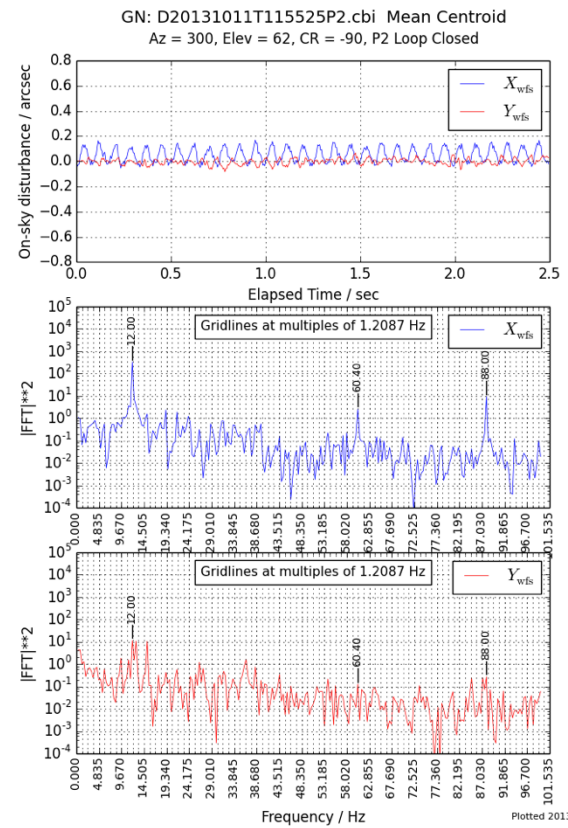
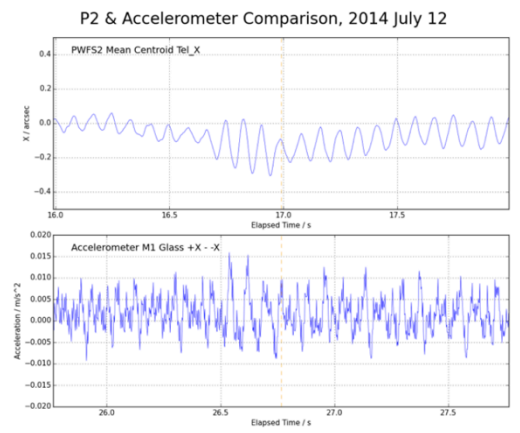
- History and source of Vibration at Gemini North
- Auto-guider and control loop
- Fast tip-tilt secondary mirror
- Closed loop vibration tracking
- Performance and results
- Real-time monitoring

# 12 Hz Vibration at M1 Can Distort Wavefront ~40%



## Cryocooler-induced Telescope Optical Vibrations

- Gemini North images have been known to exhibit strong elongations.
- WFS data analysis reveal 12 Hz sinusoidal oscillation: ~100 mas, parallel to elevation (X) axis

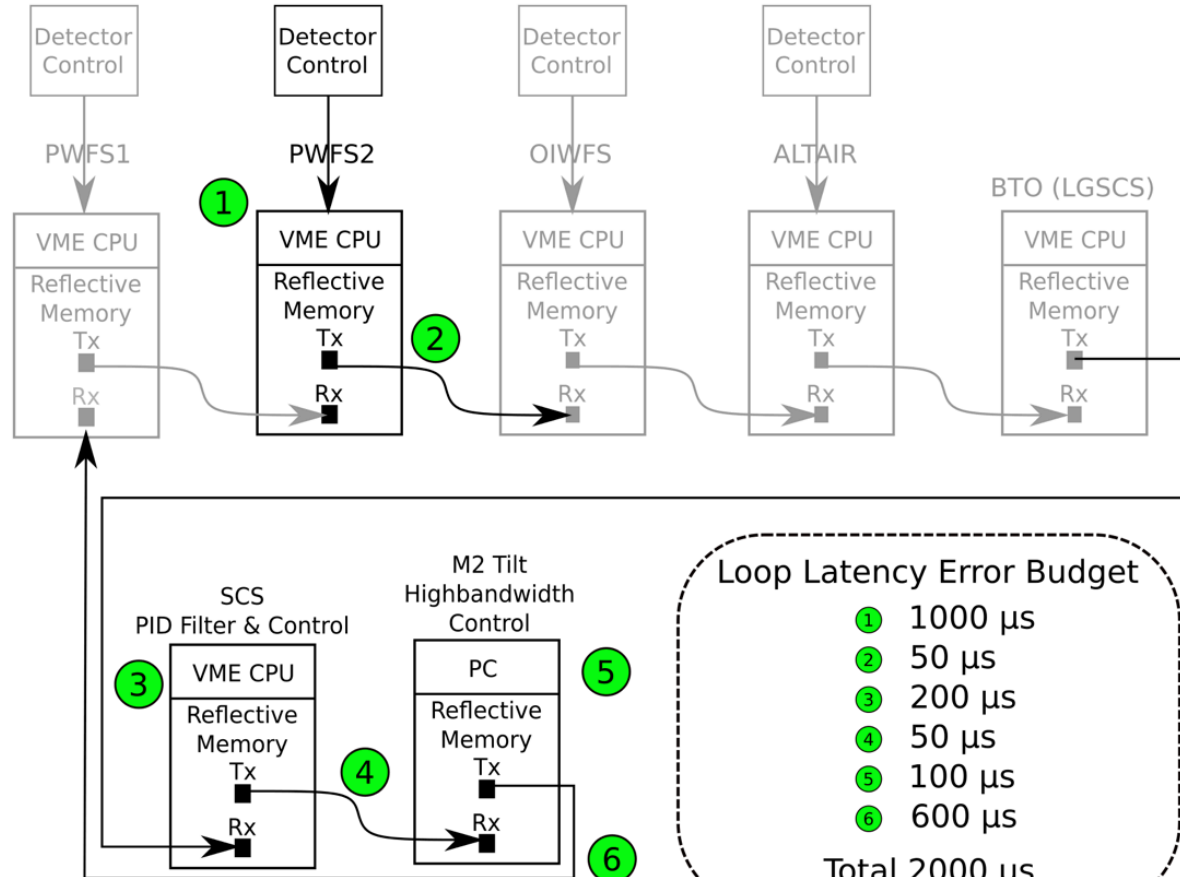


Amplitude correlates with GNIRS coldhead stroke parallel to X axis. 12 Hz amplitude absent parallel to Y.

# Auto-guider at Gemini

## Process Flow

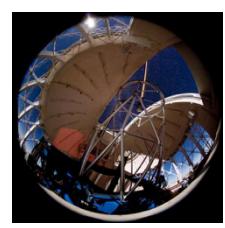
- 1 -- Start reading CCD
- 2 -- Calculate centroids
- 3 -- Calculate Zernike coeffs.
- 4 -- Write coefficients into A&G Reflective Memory
- 5 -- Interrupt M2 VME Reflective Memory
- 6 -- Read coefficients from M2 VME Reflective Memory
- 7 -- Calculate position desired for M2 Tilt / Translation
- 8 -- Write demands out to M2 Tilt Reflective Memory
- 9 -- Interrupt M2 Tilt Reflective Memory
- 10 -- Read coefficients from M2 Tilt Reflective Memory
- 11 -- Calculate voltages required on M2 tilt actuators
- 12 -- Generate voltage on actuators
- 13 -- Contingency



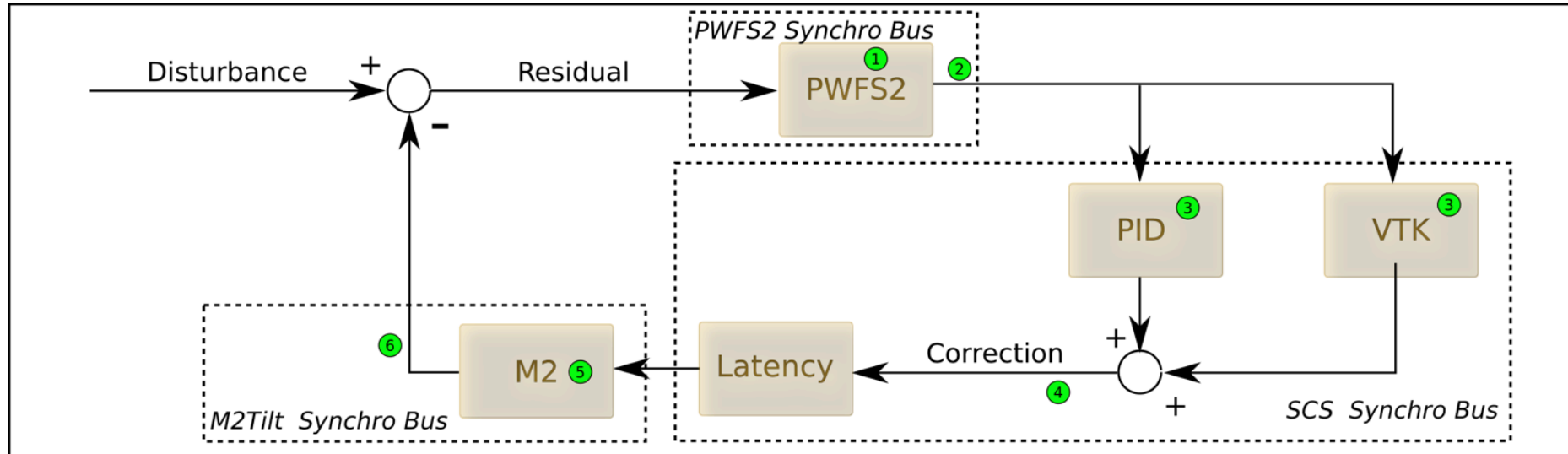
## Loop Latency Error Budget

- 1 1000  $\mu$ s
- 2 50  $\mu$ s
- 3 200  $\mu$ s
- 4 50  $\mu$ s
- 5 100  $\mu$ s
- 6 600  $\mu$ s

Total 2000  $\mu$ s



# Closed Loop Model



# VTK Model

1. Define complex **phase** oscillator:  $R_k = e(-j\theta_k)$   
 where  $\theta_k = 2\pi \frac{F_0}{F_s}$   
 $F_0$  is initial vibration tracking frequency 12 Hz  
 $F_s$  the sample rate of the autoguider = 200 Hz  
 $R_k$  is advanced through  $\theta$  at each cycle  $k$

2. The input vibration signal  $S_k$  is projected on the oscillator and accumulated in the complex **amplitude** with a gain  $G_a$ .

$$A_k = A_{k-1} + G_a R_k S_k$$

3. Vibration compensated by commanding M2

$$C_k = -2 * \text{real}(\text{conj}(A_k) * R_k * A_{PID})$$

4. **Frequency** Tracking

$$\delta\varphi_k = \varphi_k - \varphi_{k-1} \quad \text{find phase change}$$

$$\delta F_k = \frac{\delta\varphi_k}{2\pi} F_s \quad \text{scale to frequency}$$

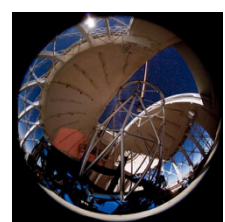
$$F_{k+1} = F_k - G_F \delta F_k \quad \text{filter frequency tracking calculated for next cycle } k+1$$

$$\theta_{k+1} = \frac{2\pi F_{k+1}}{F_s} \quad \text{phase angle for next cycle tracks the frequency of vibration.}$$

Initialize  $R_k =$

$$\begin{bmatrix} \cos \theta_k & -\sin \theta_k \\ \sin \theta_k & \cos \theta_k \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

- If the amplitude of  $S_k$  (the 12 Hz vibration signal) goes to zero, the commanded VTK amplitude also goes to zero!
- With the sample rate  $F_s = 200$  Hz we can track the frequency of the vibration by monitoring the phase change from the current and previous cycle.

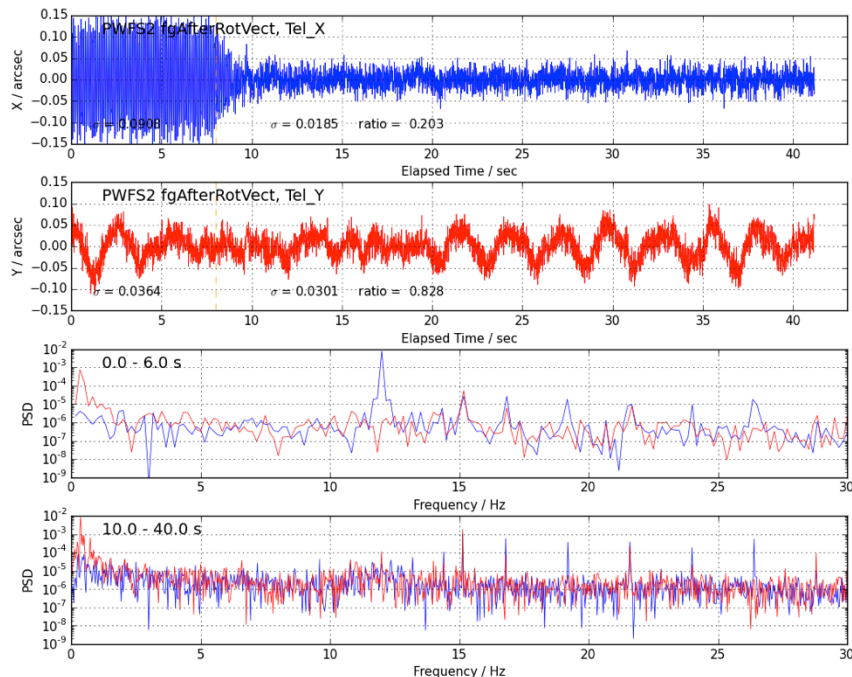


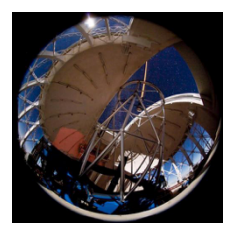
# Results



- VTK is capable of rejecting the 12Hz vibration of M1 induced by harmonics in the GNIRS cold heads.
- Control methods may help reject the most prominent harmonics, but this does not remove the vibrations.
- During commissioning a real-time spectrum analyzer was developed to monitor the health of the VTK. See QRcodes for YouTube demo.
- Graph shows convergence as operators assert VTK.

VTK Test w/ PWFS2, 200 Hz, CRPA = -90 : 2015 Apr 24, D20150424T075214P2.cbcbfg





# Thank you!

